



**AMENDMENTS TO THE CLAIMS:**

This listing of claims will replace all prior versions, and listings, of claims in the application:

**LISTING OF CLAIMS:**

1. (Withdrawn) Method of depositing a crystalline  $\alpha$ - $\text{Al}_2\text{O}_3$ -layer onto a cutting tool insert by chemical vapor deposition comprising the following steps:

depositing a from about 0.1 to about 1.5  $\mu\text{m}$  layer of  $\text{TiC}_x\text{N}_y\text{O}_z$  where  $x+y+z \geq 1$  and  $z > 0$ ;

treating said layer at from about 625 to about 1000  $^\circ\text{C}$  in a gas mixture containing from about 0.5 to about 3 vol-%  $\text{O}_2$  for a short period of time from about 0.5 to about 4 min; and

depositing said  $\text{Al}_2\text{O}_3$ -layer by bringing said treated layer into contact with a gas mixture containing from about 2 to about 10 vol-% of  $\text{AlCl}_3$ , from about 16 to about 40 vol-% of  $\text{CO}_2$ , in  $\text{H}_2$  and from about 0.8 to about 2 vol-% of a sulphur--containing agent at a process pressure of from about 40 to about 300 mbar and a temperature of from about 625 to about 800  $^\circ\text{C}$ .

2. (Withdrawn) The method of claim 1 wherein  
in said depositing a from about 0.1 to about 1.5  $\mu\text{m}$  layer of  $\text{TiC}_x\text{N}_y\text{O}_z$ ,  $x+y+z \geq 1$  and  $z > 0.2$ ;

in said treating said layer at from about 625 to about 1000 °C in a gas mixture containing O<sub>2</sub>, said O<sub>2</sub> is present as CO<sub>2</sub> + H<sub>2</sub> or O<sub>2</sub> + H<sub>2</sub> and said treating occurs for a short period of time from about 0.5 to about 4 min; and

in said depositing said Al<sub>2</sub>O<sub>3</sub>-layer, the temperature is from about 625 to 700 °C.

3. (Withdrawn) The method of claim 2 wherein the depositing temperature is from about 650 to 695 °C.

4. (Withdrawn) The method of claim 1 wherein said treating step is also carried out in the presence of from about 0.5 to about 6 vol-% HCl.

5. (Previously Presented) Cutting tool comprising a body with, at least on functioning parts of a surface of the body, a hard and wear resistant coating comprising at least one layer consisting essentially of crystalline  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> with a thickness of from about 0.5 to about 10  $\mu$ m, said crystalline  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> having columnar grains with an average grain width of from about 0.1 to about 1.1  $\mu$ m and being deposited by chemical vapor deposition at a temperature of from about 625 to about 800 °C.

6. (Previously Presented) The cutting tool of claim 19 wherein said body comprises a body of cubic boron nitride or diamond.

7. (Original) The cutting tool of claim 5 wherein said coating comprises at least one layer consisting of  $\text{Ti}(\text{C},\text{N})$  with a thickness of from about 0.5 to about 10  $\mu\text{m}$  deposited between the body and said  $\alpha\text{-Al}_2\text{O}_3$ -layer by the MTCVD technique at a temperature less than 885 °C.

8. (Original) The cutting tool according to claim 7 wherein said coating further comprises an intermediate layer of from about 0.5 to about 1.5  $\mu\text{m}$  of  $\text{TiC}_x\text{N}_y\text{O}_z$  where  $x+y+z \geq 1$  and  $z > 0$  between the  $\alpha\text{-Al}_2\text{O}_3$ -layer and the MTCVD-TiCN-layer.

9. (Original) The cutting tool according to claim 8 wherein in said intermediate layer  $z > 0.2$ .

10. (Original) The cutting tool according to claim 9 wherein in said coating intermediate layer  $z > 0.2$ ,  $y = 0$  and  $x \geq 0$ .

11. (Original) The cutting tool of claim 5 wherein said coating comprises at least one layer adjacent to the tool body deposited by PVD or PACVD.

12. (Original) The cutting tool of claim 11 wherein said coating comprises an intermediate layer of from about 0.1 to about 1.5  $\mu\text{m}$   $\text{TiC}_x\text{N}_y\text{O}_z$  between the  $\alpha\text{-Al}_2\text{O}_3$  and the PVD or PACVD-layer(s,) where  $x+y+z \geq 1$  and  $z > 0$ .

13. (Original) The cutting tool of claim 12 wherein in said intermediate layer  $z > 0.2$ .

14. (Original) The cutting tool of claim 13 wherein in said intermediate layer  $z > 0.2$ ,  $y \geq 0$  and  $x < 0.1$ .

15. (Original) The cutting tool of claim 11 wherein said coating has a pronounced columnar grain structure with a grain width of  $< 0.5 \mu\text{m}$ .

16. (Previously Presented) The cutting tool of claim 5 wherein one such  $\alpha\text{-Al}_2\text{O}_3$  layer is a top visible layer at least along a cutting edge line.

17. (Previously Presented) The cutting tool of claim 5 wherein the coating on a rake face and along an edge line has been smoothed by brushing or by blasting to a surface roughness,  $R_{a1}$  of less than  $0.2 \mu\text{m}$  over a measured length of  $5 \mu\text{m}$ .

18. (Withdrawn) The cutting tool of claim 5 wherein said tool is a cutting insert, a solid carbide drill or a carbide end-mill.

19. (Previously Presented) The cutting tool of claim 5, wherein the body comprises sintered cemented carbide, cermet, ceramic, high speed steel or superhard materials.

20. (Previously Presented) A cutting tool comprising:

a body including a plurality of functioning parts on a surface of the body;

a hard and wear resistant coating on at least the functioning parts,

wherein the body comprises cubic boron nitride or diamond,

wherein the coating comprises at least one layer consisting essentially of crystalline  $\alpha$ - $\text{Al}_2\text{O}_3$  with a thickness of from about 0.5 to about 10  $\mu\text{m}$ , the crystalline  $\alpha$ - $\text{Al}_2\text{O}_3$  having columnar grains with an average grain width of from about 0.1 to about 1.1  $\mu\text{m}$  and being deposited by chemical vapor deposition at a temperature of from about 625 to about 800  $^\circ\text{C}$ , and

wherein said coating comprises at least one layer consisting of  $\text{Ti}(\text{C},\text{N})$  with a thickness of from about 0.5 to about 10  $\mu\text{m}$  deposited between the body and said  $\alpha$ - $\text{Al}_2\text{O}_3$ -layer.

21. (Previously Presented) The cutting tool of claim 20, wherein said coating further comprises an intermediate layer of from about 0.5 to about 1.5  $\mu\text{m}$  of  $\text{TiC}_x\text{N}_y\text{O}_z$  between the  $\alpha$ - $\text{Al}_2\text{O}_3$ -layer and the  $\text{Ti}(\text{C},\text{N})$ -layer, where  $x+y+z=1$  and  $z>0$ .